

Non-Linear Aeroelastic Modelling and Prediction

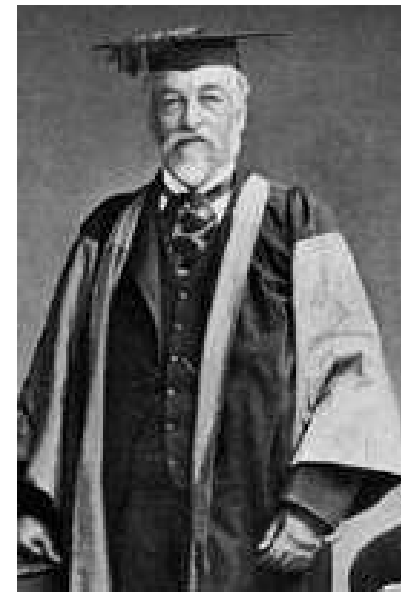
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Outline

- Overview of Aeroelasticity
- Outline of several aeroelastic phenomena
- Flutter
 - Prediction of stability bounds
- Effect of non-linearities
 - Structural
 - Aerodynamic
 - Control system
- Limit Cycle Oscillations
 - Determination of LCO characteristics
- Future Directions

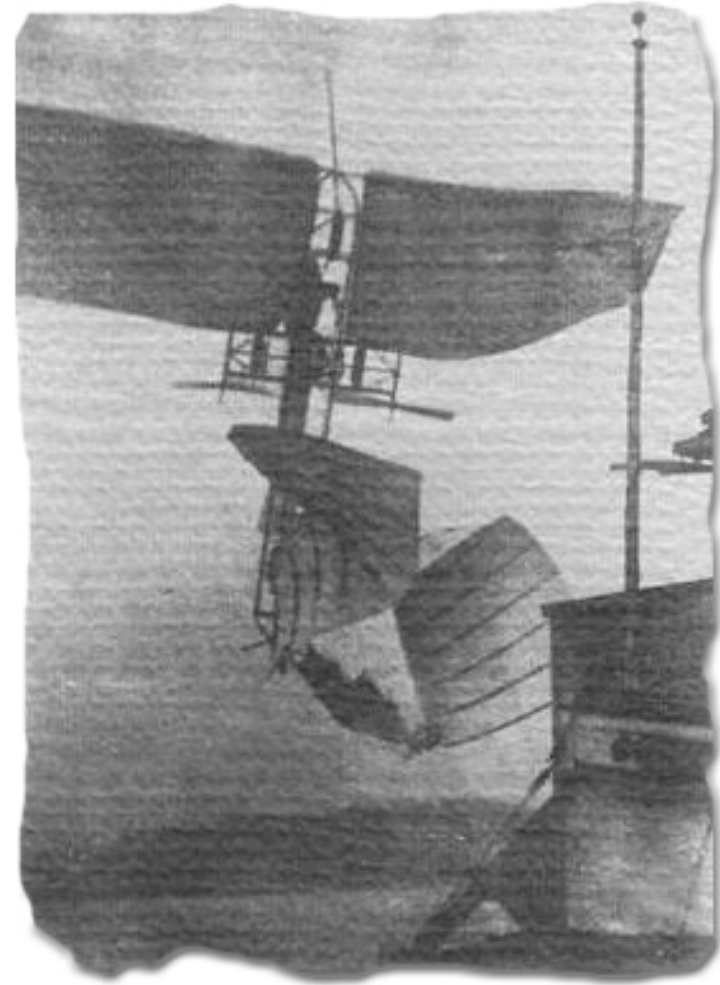
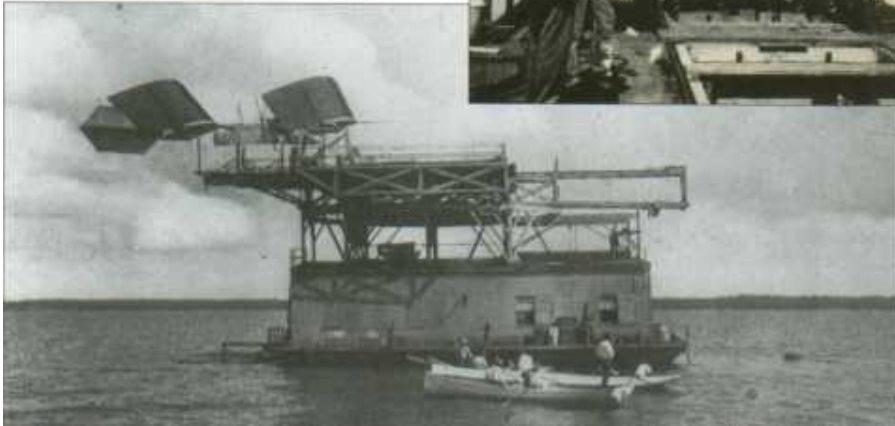
104 Years Ago in the USA

- Wright brothers were perfecting their “Flyer” at Kitty Hawk.
- Samuel Langley, backed by the Smithsonian Institute, attempted to fly his “Aerodrome” off a houseboat on the Potomac River.



Langley's Tests

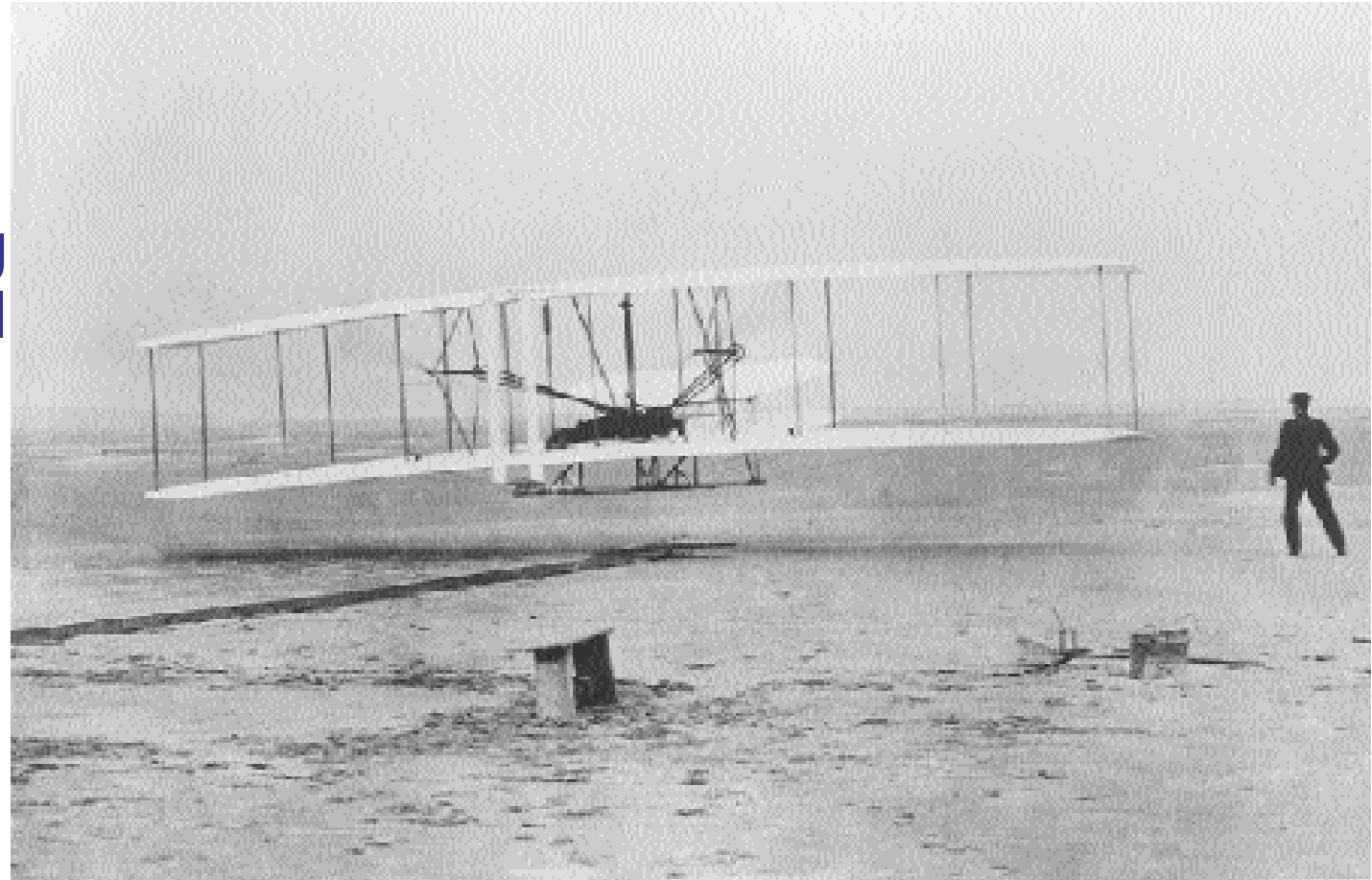
- Structural failure



- Success

- Wing warping for roll control

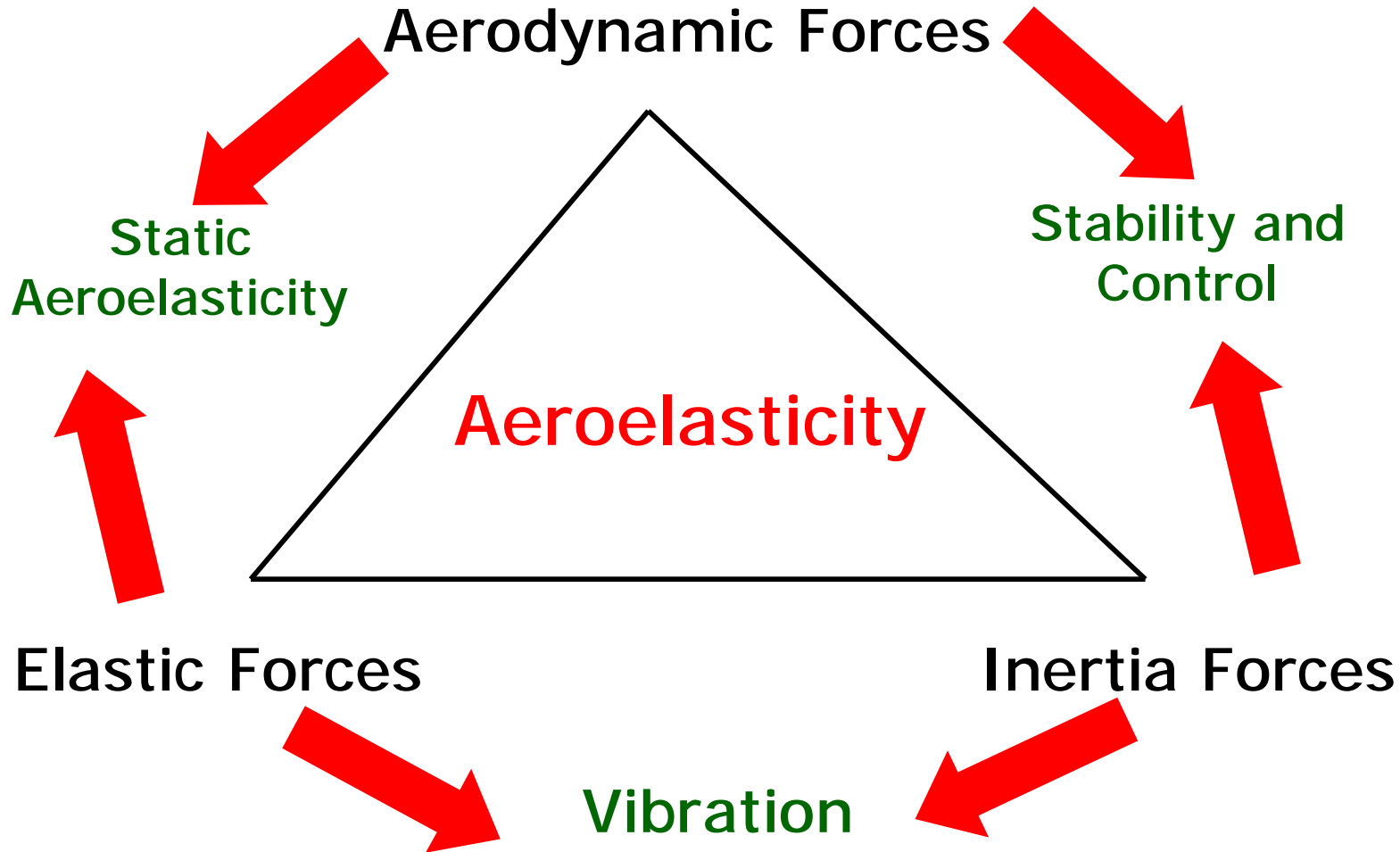
Wright Brothers



Langley - First Known Aeroelastic Failure

- Wings were not stiff enough
- “Divergence” – torsional loads overcome structural restoring forces
- “Aerodrome” rebuilt some years later by Curtis with stiffer wings – it flew
- Interaction of flexible structure and aerodynamic forces need to be considered
- Science of **Aeroelasticity**

Collar's Aeroelastic Triangle



Aeroelastic Phenomena

- Mostly undesirable
- Often catastrophic
 - Flutter / Divergence
- Response
 - Gusts / Manoeuvres / Control surface inputs
 - Buffet
- Linear and non-linear response
- Key criteria for aircraft design and certification
 - Many (1000s) of cases need to be considered
- Still unable to accurately predict some types of behaviour



F-18 HARV
Smoke Test
late 1980's
 Dryden
 Flight Research Center

Aeroelastic Equations

$$\underbrace{A}_{\text{Inertia}} \ddot{y} + \underbrace{(\rho V B + D)}_{\text{Aerodynamic Damping}} \dot{y} + \underbrace{(\rho V^2 C + E)}_{\text{Aerodynamic Stiffness}} y = \underline{0}$$

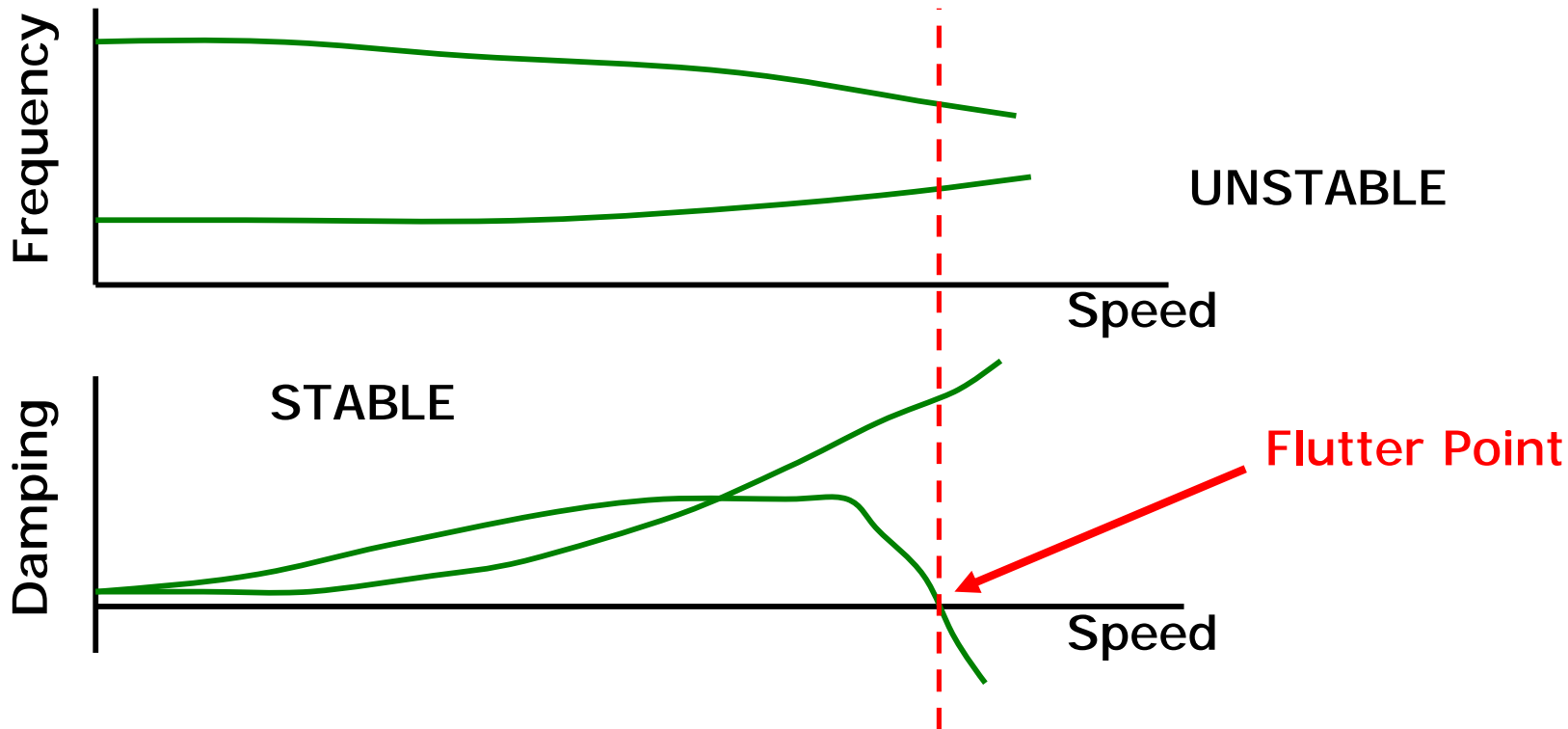
Structural Damping

Structural Stiffness

- 2nd order differential equation cf. $M \ddot{x} + C \dot{x} + K x = \underline{0}$
- Stiffness and damping change with speed and height
- Matrices of order 80 x 80
- Right hand side for gusts / control inputs

Flutter

- Violent unstable vibration often resulting in structural failure
- Two modes interact with each other



Aeroelasticity at its Worst



- Aeroelastic equations

$$\underline{\mathbf{A}} \dot{\underline{\mathbf{q}}} + (\rho V \mathbf{B} + \mathbf{D}) \underline{\mathbf{q}} + (\rho V^2 \mathbf{C} + \mathbf{E}) \underline{\mathbf{q}} = \underline{\mathbf{0}}$$

- First order form

$$\begin{Bmatrix} \dot{\underline{\mathbf{q}}} \\ \underline{\mathbf{q}} \end{Bmatrix} - \begin{bmatrix} \mathbf{0} & \mathbf{I} \\ -\mathbf{A}^{-1}(\rho V^2 \mathbf{C} + \mathbf{E}) & -\mathbf{A}^{-1}(\rho V \mathbf{B} + \mathbf{D}) \end{bmatrix} \begin{Bmatrix} \underline{\mathbf{q}} \\ \underline{\mathbf{q}} \end{Bmatrix} = \underline{\mathbf{0}}$$

- Eigenvalue problem

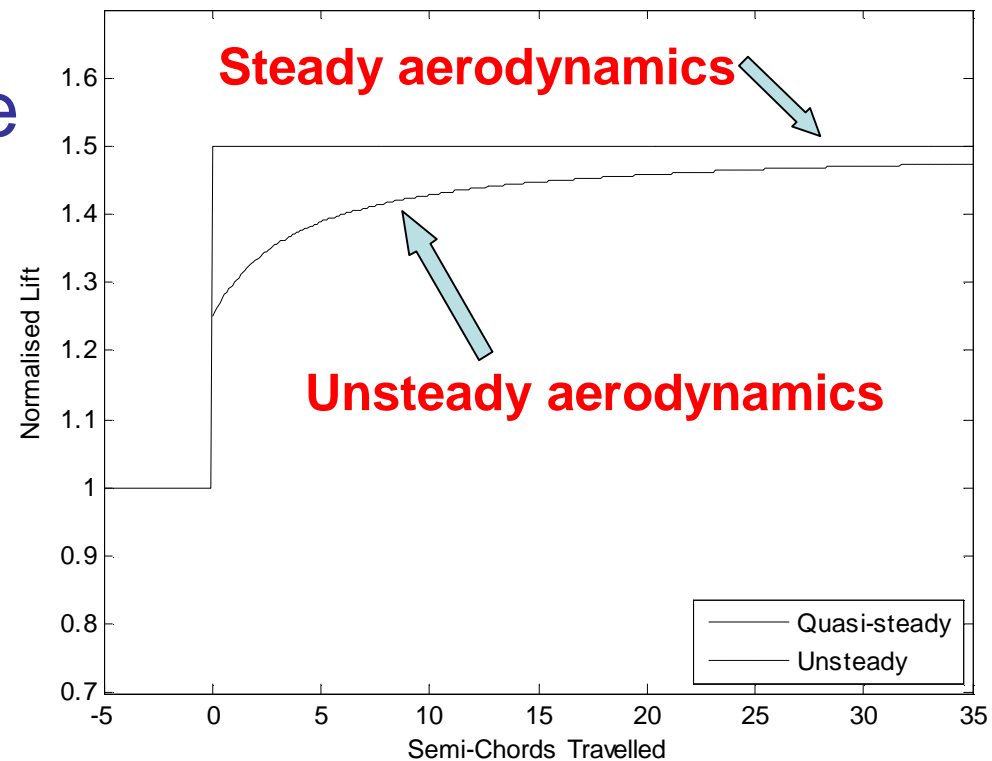
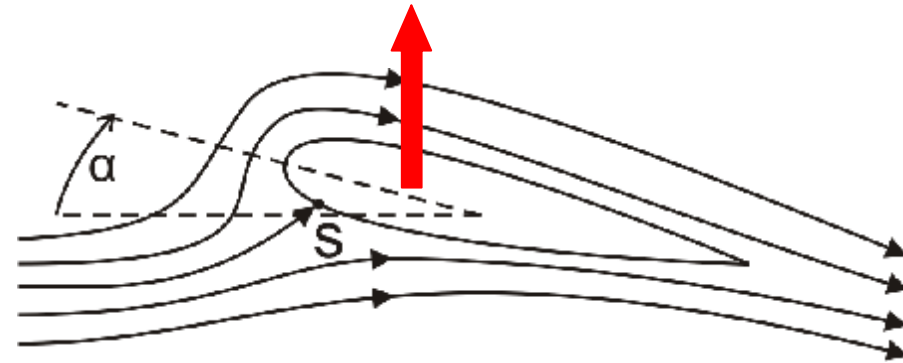
$$\underline{\mathbf{Q}} \underline{\mathbf{x}} = \underline{\mathbf{0}} \quad \underline{\mathbf{x}} = \underline{\mathbf{x}}_0 e^{\lambda t} \quad \longrightarrow \quad (\mathbf{Q} - \mathbf{I}\lambda) \underline{\mathbf{x}}_0 = \underline{\mathbf{0}}$$

- Eigenvalues of Q

$$\lambda_j = -\zeta_j \omega_j \pm i \omega_j \sqrt{1 - \zeta_j^2} \quad j = 1, 2 \mathbf{K} \mathbf{N}$$

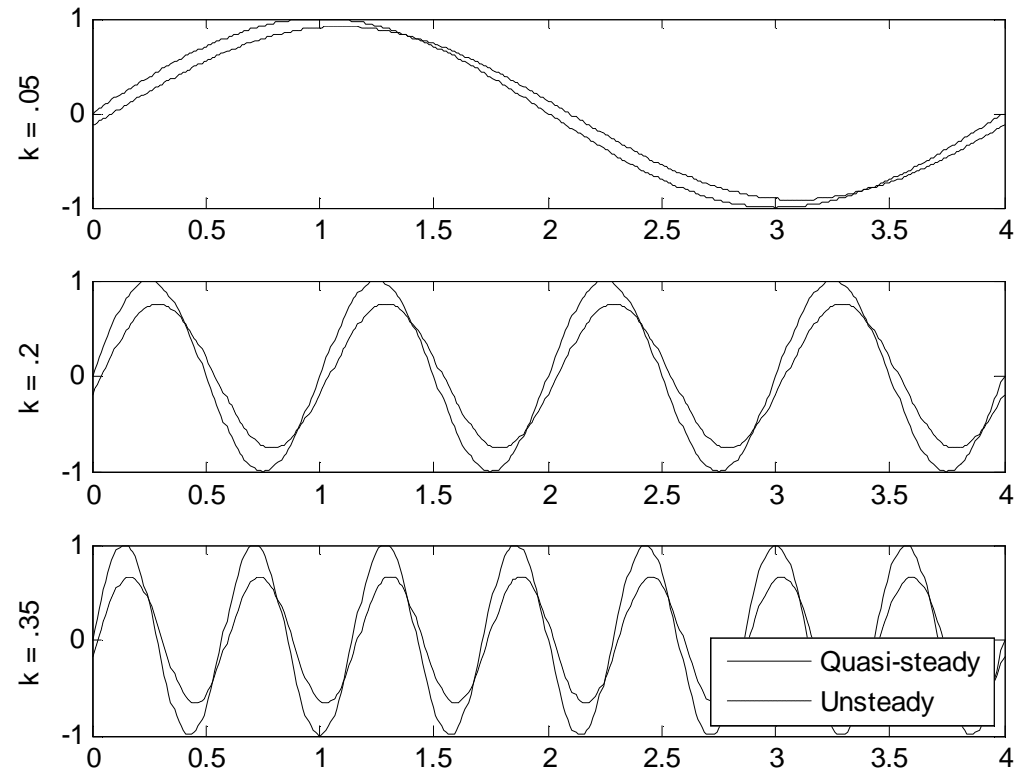
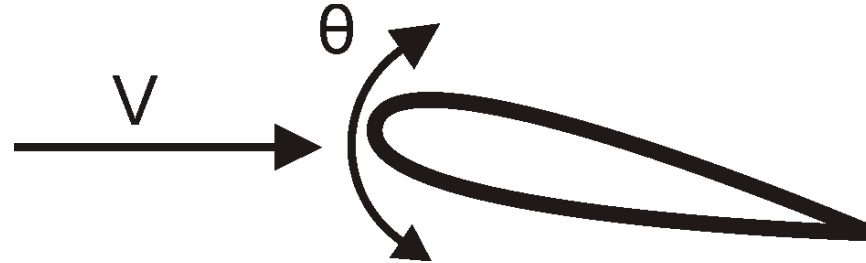
Unsteady Aerodynamics

- Steady lift proportional to angle of incidence
- Consider sudden change in incidence



Effect of Harmonic Motion

- Oscillatory motion of aerofoil
 - Lift depends upon the reduced frequency
- $$k = \frac{\omega b}{V} = \frac{\omega c}{2V}$$
- B and C are reduced frequency dependent



Frequency Matching

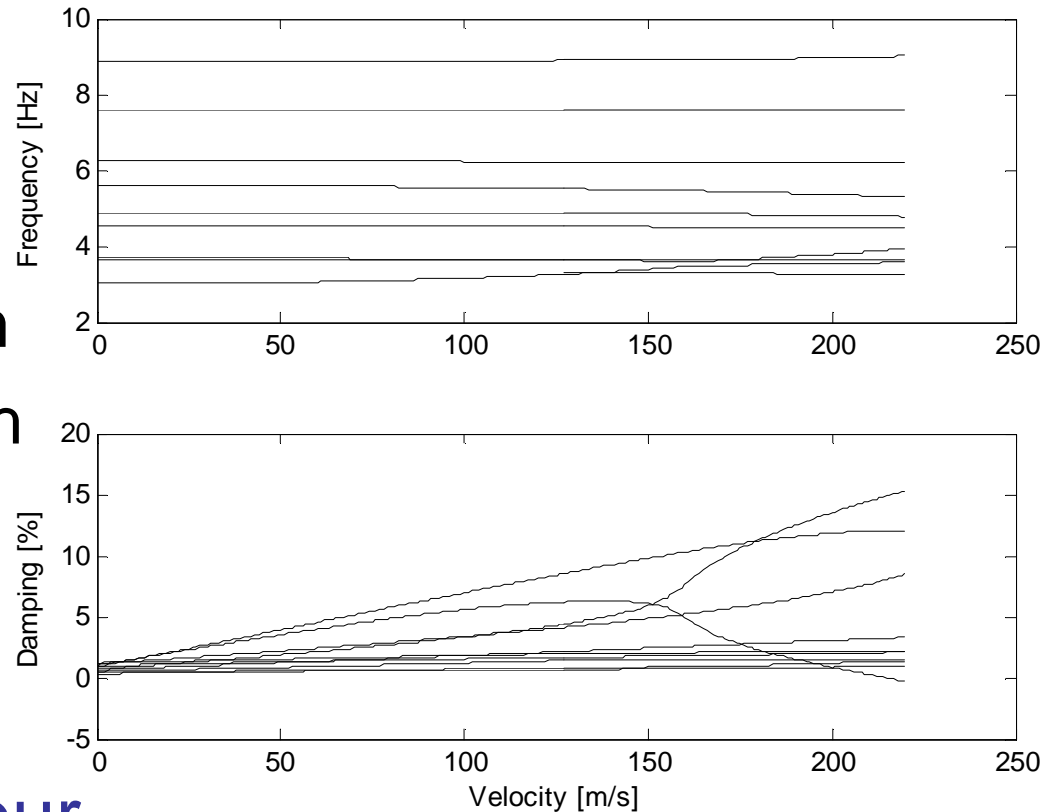
- Aeroelastic equations

$$\underline{\mathbf{A}}\underline{\dot{\mathbf{q}}} + (\rho V \underline{\mathbf{B}} + \underline{\mathbf{D}})\underline{\dot{\mathbf{q}}} + (\rho V^2 \underline{\mathbf{C}} + \underline{\mathbf{E}})\underline{\mathbf{q}} = \underline{\mathbf{0}}$$

- If A,B,C,D,E are known
 - Typically using “panel methods”
 - Find ω and ζ from eigen problem
- But, need to know ω and ζ
 - To find B and C
- “Chicken and Egg” situation
 - Frequency matching problem
 - Consider individual harmonics

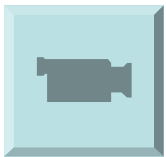
PK Method

- At each speed and frequency
 - Guess frequency
 - Calculate B and C
 - Solve eigenproblem
 - Repeat process with new frequency
- Exact at flutter condition
- Sub-critical behaviour not exact



Control Surface Flutter

- Interaction of control surface and wing
- F-117 Stealth Fighter
 - Freeplay of control surfaces

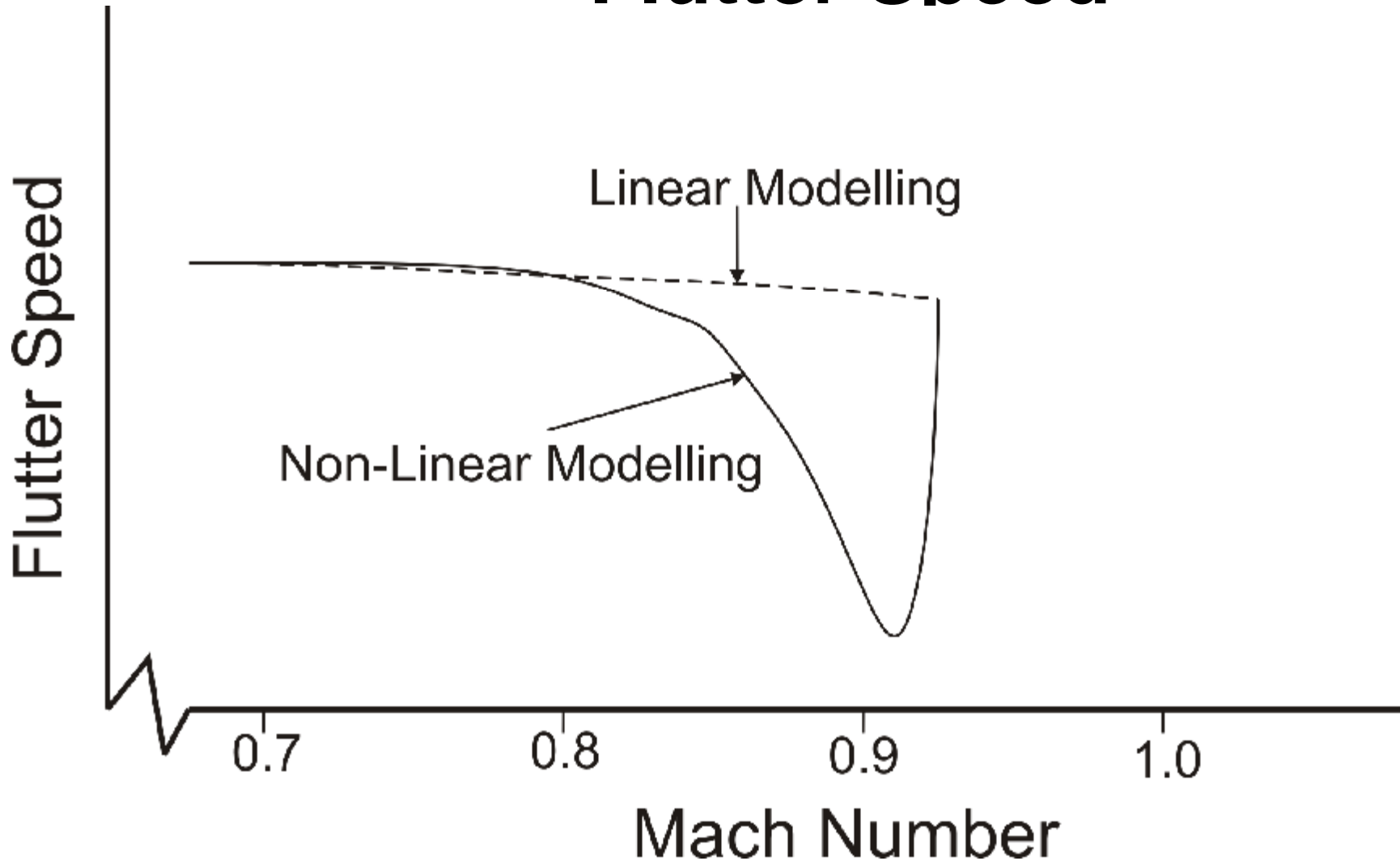


Effect of Non-Linearities

- Non-linear phenomena change aeroelastic behaviour
 - Structural
 - Cubic stiffening - joints
 - Freeplay – control surfaces
 - Aerodynamic
 - Transonic behaviour
 - Moving shocks
 - Stall flutter
 - Control
 - Control surface rate and deflection limits
 - Control circuit time delays



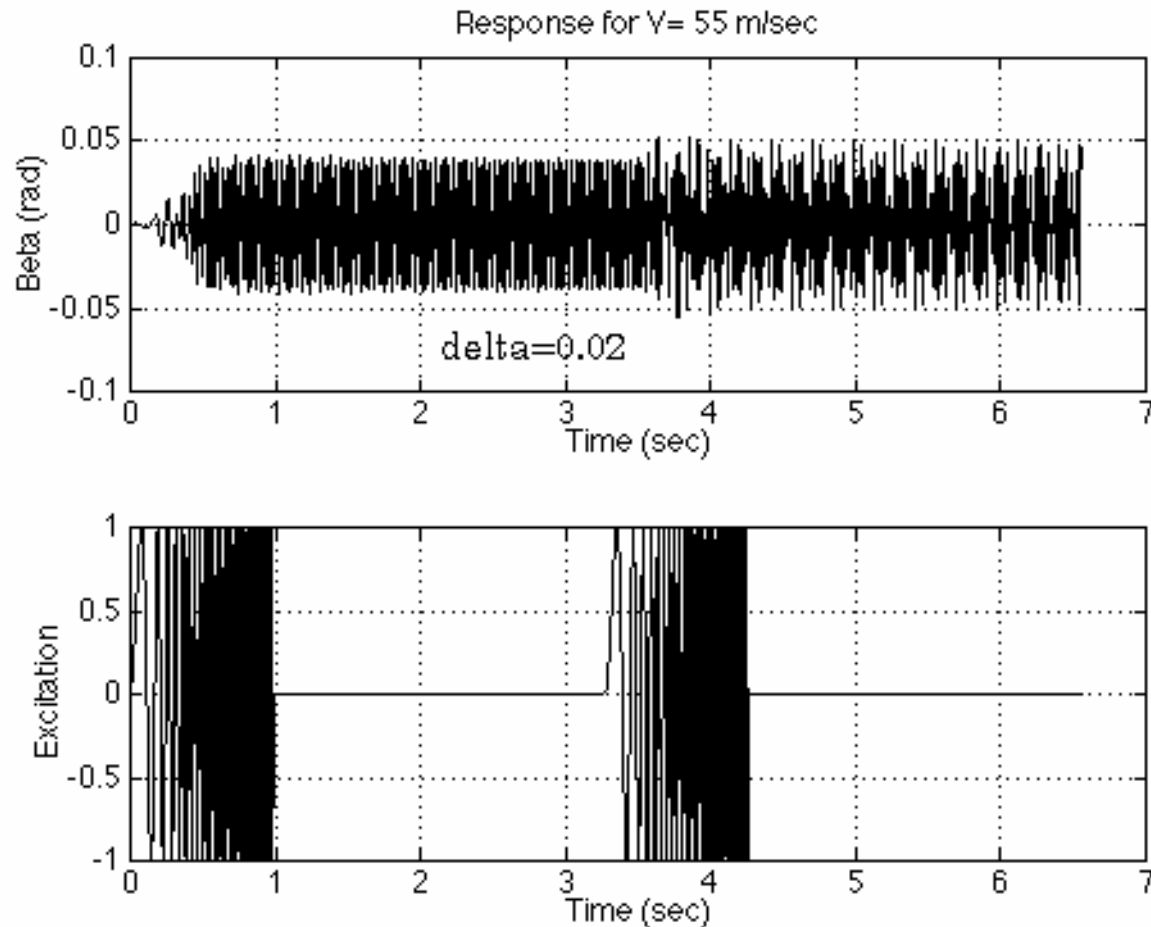
Effect of Transonic Flow on Flutter Speed



Need high fidelity aerodynamics to model accurately

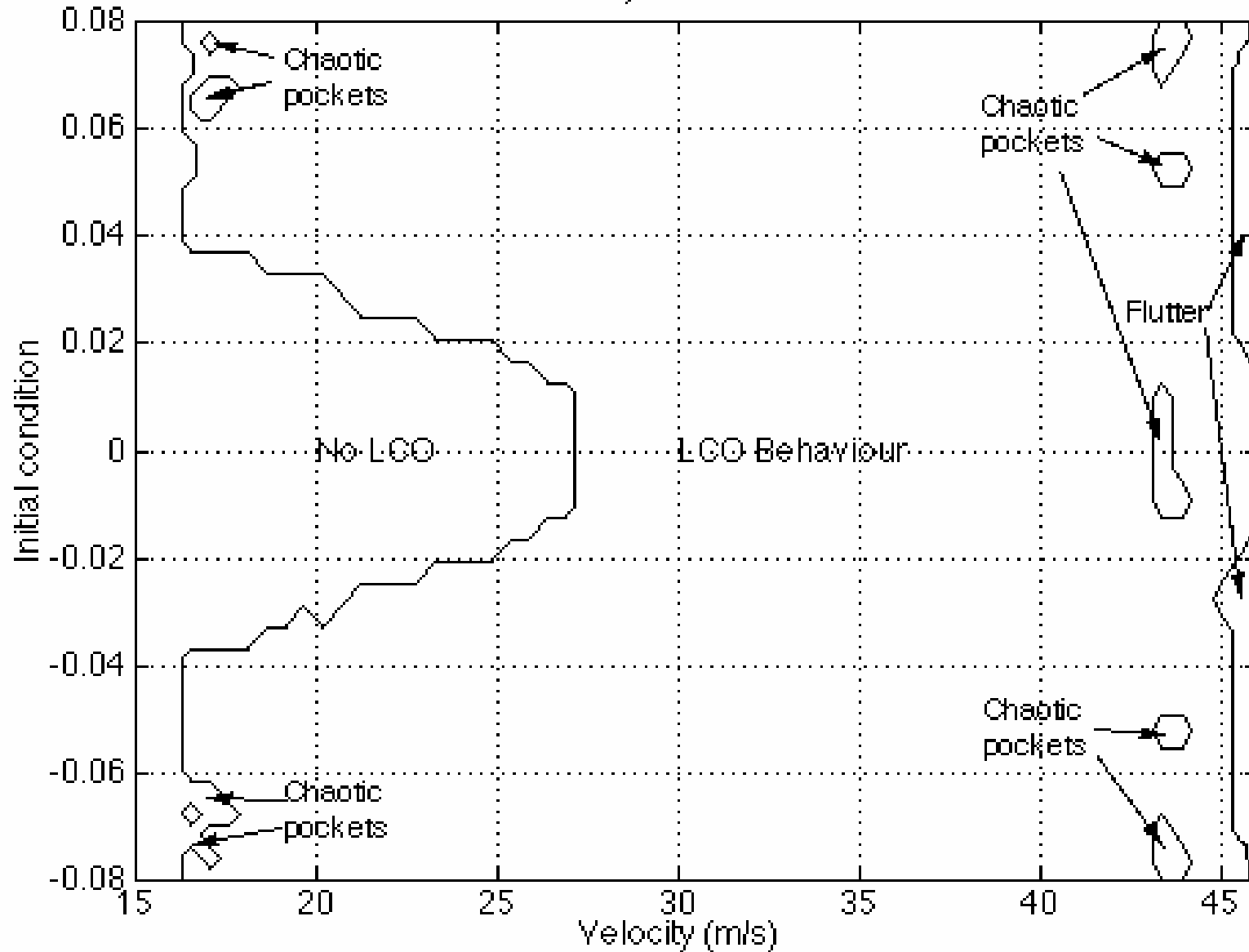
Limit Cycle Oscillations

- Non-linearities cause a bounded flutter to occur
- Not disastrous
 - Fatigue problem
 - Other problems
 - weapon aiming
 - pilot control

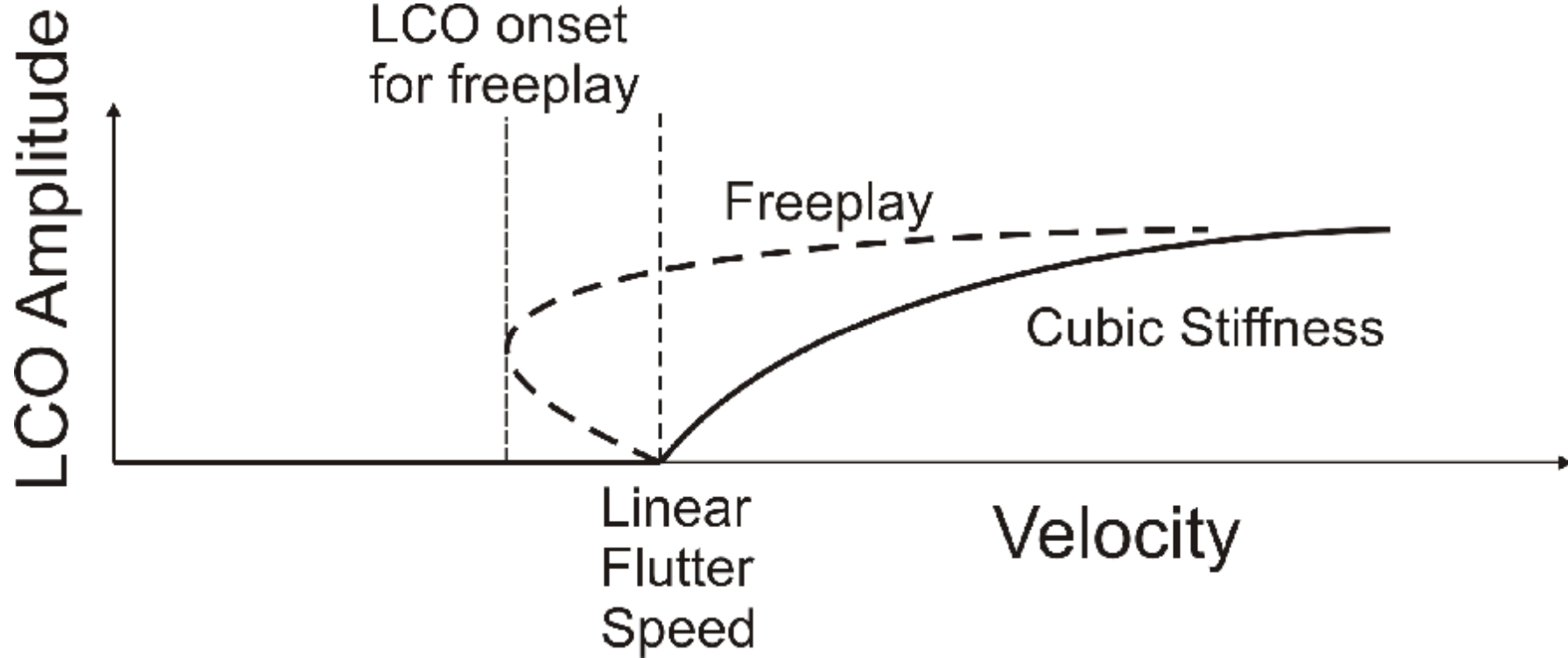


Typical Parameter Space Behaviour

Limit Cycle existence



LCO Amplitude Behaviour



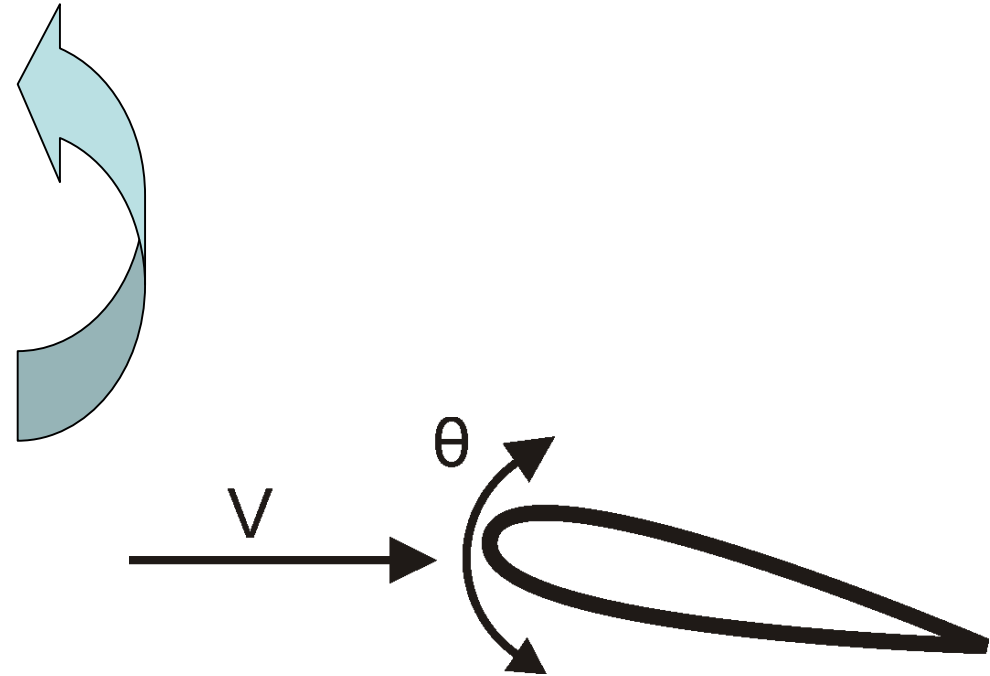
Limit Cycle Oscillations

- Interaction of control surface and wing
- Example here is limited amplitude
 - Limit Cycle Oscillation (LCO)



Stall Flutter

- If angle of incidence gets too high
 - Flow separates
 - Lift is lost
 - Incidence reduces
 - Flow reattaches
 - Incidence increases
- LCO results
- Occurs at wing tips



Military Aircraft with Stores

- Cannot predict LCO using current methods
- Problems if unpredicted vibration occurs in flight test
- Lots of (expensive) testing needed



USAF Photo

Prediction of Stability Boundaries and Characteristics

- Possible to compute coupled FE/CFD models but very expensive in transonic region
- Many design cases need to be considered
- Aim to use non-linear dynamics methods to determine regions of interest
- Direct interesting areas where the FE/CFD analysis should be used
- Interested in
 - Stability boundaries
 - Amplitudes
 - Frequencies

- **Continuous Non-linearities (Normal Form)**
 - structural and aerodynamic non-linearities
 - determination of LCO frequencies and amplitudes
- **Discontinuous Non-linearities**
(Normal Form / Harmonic Balance methods / Cell Mapping / numerical continuation)
 - structural and control system non-linearities

Aeroelastic Equations of Motion

$$\underline{\mathbf{A}}\underline{\dot{\mathbf{q}}} + (\rho V \underline{\mathbf{B}} + \underline{\mathbf{D}})\underline{\dot{\mathbf{q}}} + (\rho V^2 \underline{\mathbf{C}} + \underline{\mathbf{E}})\underline{\mathbf{q}} + \underline{\mathbf{F}}(\underline{\mathbf{q}}, \underline{\dot{\mathbf{q}}}) = \underline{\mathbf{0}}$$

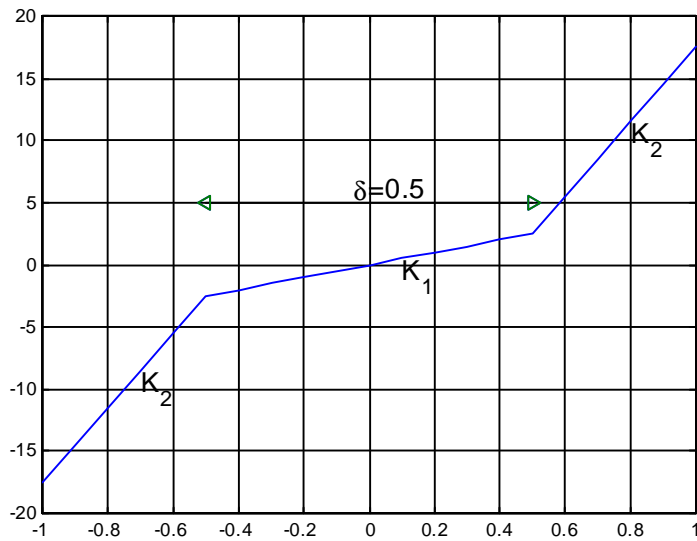
$$\begin{Bmatrix} \underline{\dot{\mathbf{q}}} \\ \underline{\mathbf{q}} \end{Bmatrix} - \begin{bmatrix} \mathbf{0} & \mathbf{I} \\ -\underline{\mathbf{A}}^{-1}(\rho V^2 \underline{\mathbf{C}} + \underline{\mathbf{E}}) & -\underline{\mathbf{A}}^{-1}(\rho V \underline{\mathbf{B}} + \underline{\mathbf{D}}) \end{bmatrix} \begin{Bmatrix} \underline{\mathbf{q}} \\ \underline{\dot{\mathbf{q}}} \end{Bmatrix} + \begin{Bmatrix} \underline{\mathbf{0}} \\ \underline{\mathbf{F}} \end{Bmatrix} = \begin{Bmatrix} \underline{\mathbf{0}} \\ \underline{\mathbf{0}} \end{Bmatrix}$$

- $\underline{\mathbf{F}}$ – nonlinearity
- Several methods used
 - Normal Form
 - Higher Order Harmonic Balance
 - Numerical Continuation

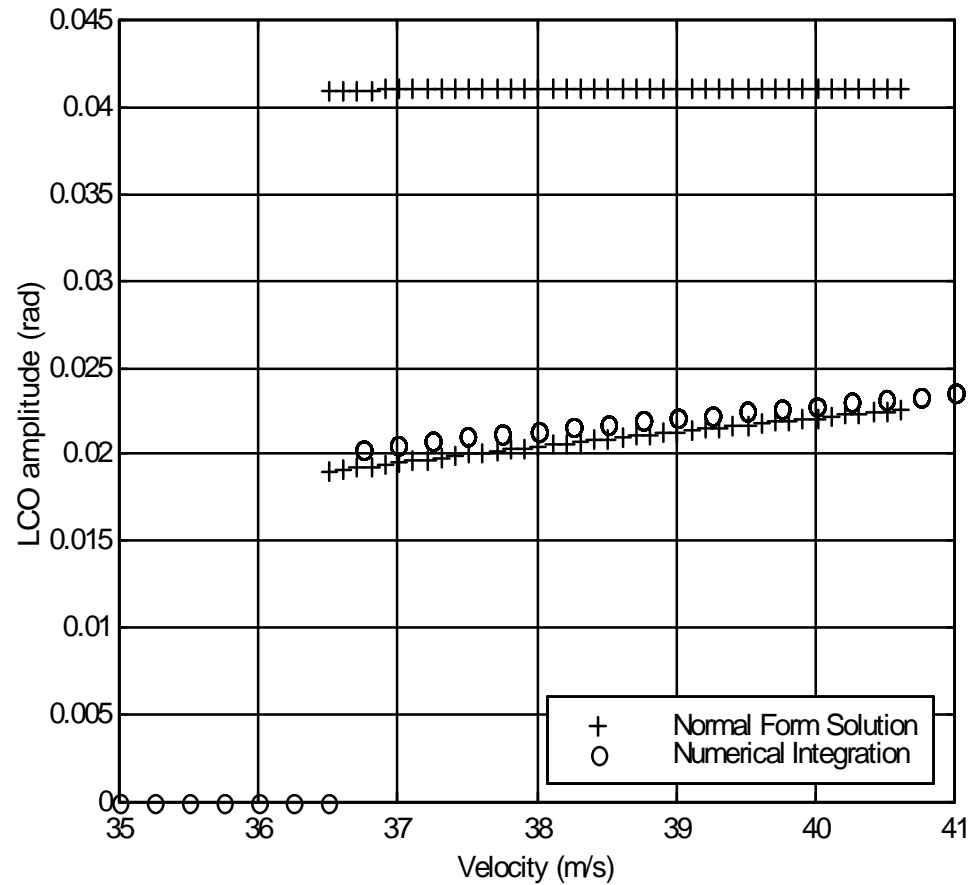
Normal Form Theory

- Technique to obtain the local post-critical behaviour on a 1DOF undergoing Hopf Bifurcation
- Requires Centre manifold theory to simplify system from MDOF to 1DOF
- Applied to structural discontinuous non-linearities
 - Curve-fit the non-linearity
 - Define the equation of motion
 - Define the linear flutter condition
 - Reduce the model (Centre Manifold)
 - Apply Normal Form Theory
 - Determine amplitude and frequency of LCO

- 18 DOF aeroelastic model
- Bi-linear non-linearity with various ratio of inner / outer stiffness



NFT Solution

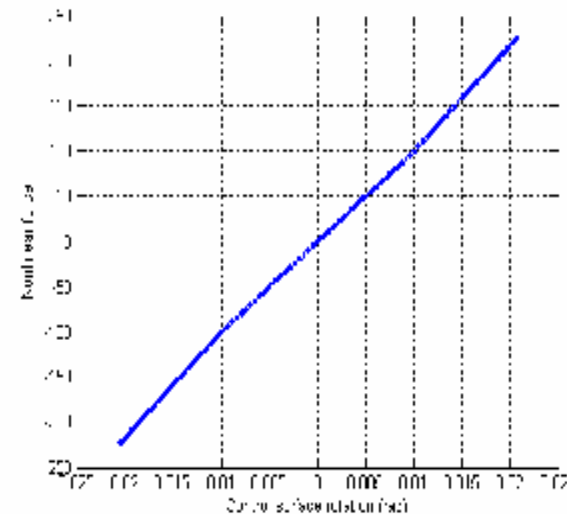
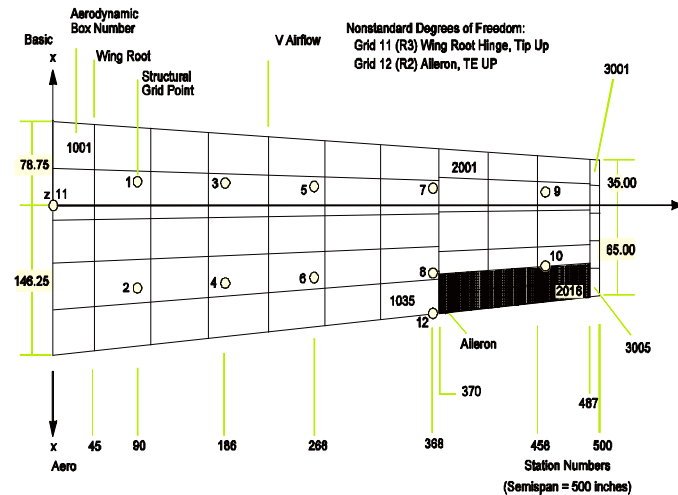


Higher Order Harmonic Balance

- Various types of bifurcation can be treated using Harmonic Balance methods
 - Hopf (sub-critical and super-critical)
 - Period Doubling
 - Folds
- Harmonic Balance
 - Approximates LCO with single sinusoidal component
 - Implementation
 - Describing function
 - Equivalent linearisation
 - Accuracy reduced if significant higher order components exists
- Higher Order Harmonic Balance
 - Similar to HB but higher order terms included
 - Approximates LCO with multiple sinusoids

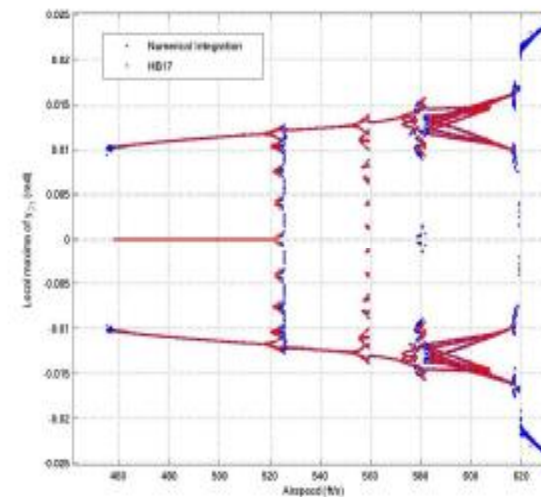
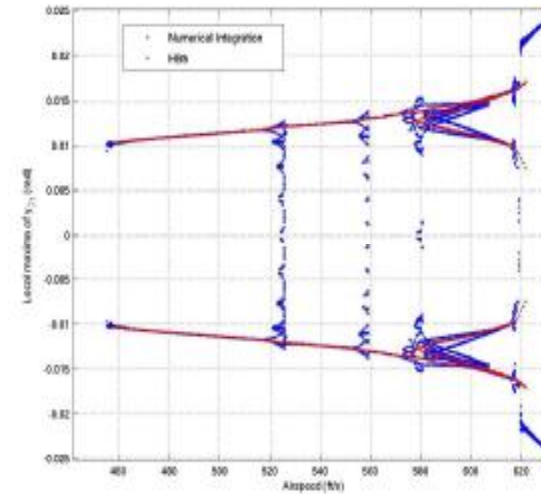
BAH Aeroelastic Model

- Bisplinghoff, Ashley and Halfman (BAH) wing
- 12 Finite Element nodes, 72 degrees of freedom
- 9 modes
- Unsteady aerodynamics with 4 aerodynamic lags
- A total of 54 states
- Piecewise linear nonlinearity in control surface rotation degree of freedom



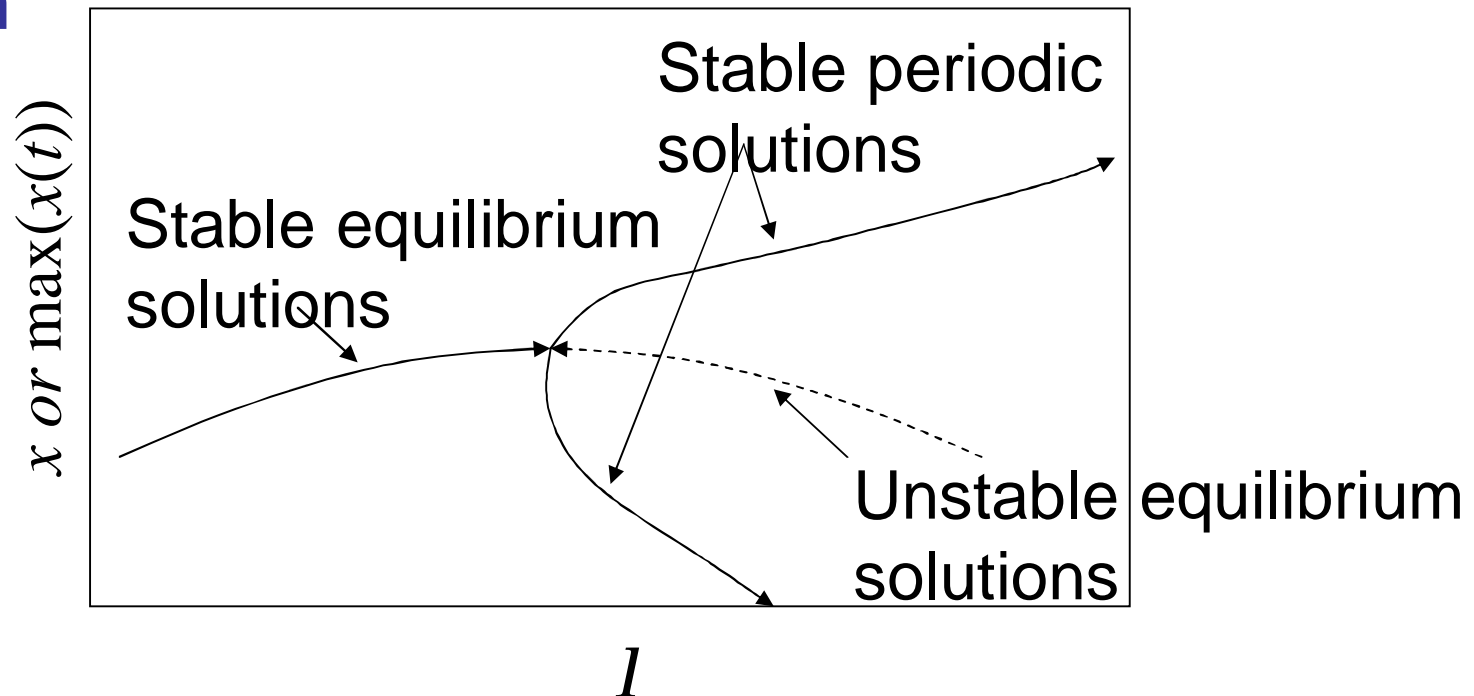
Bifurcation plots from HOHB

- Bifurcation plots from HB 5 and HB 17 for lower LCO branch
- 17th order HB results are more accurate but slower



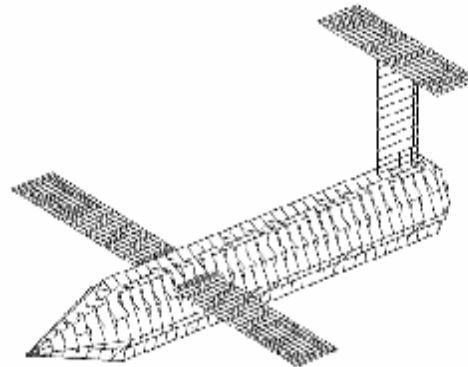
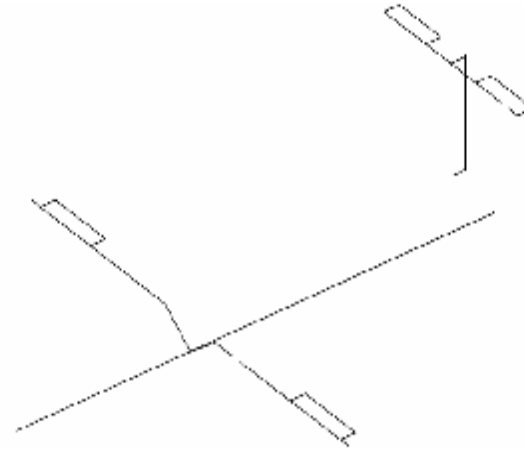
Numerical Continuation

- Numerical Continuation is a method designed to solve nonlinear algebraic equations that depend on one or more parameters
- Having achieved a solution, can then change the parameters slightly and track the new solution



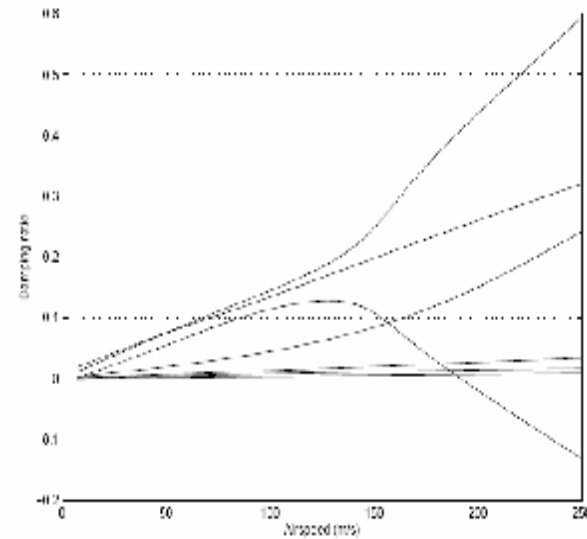
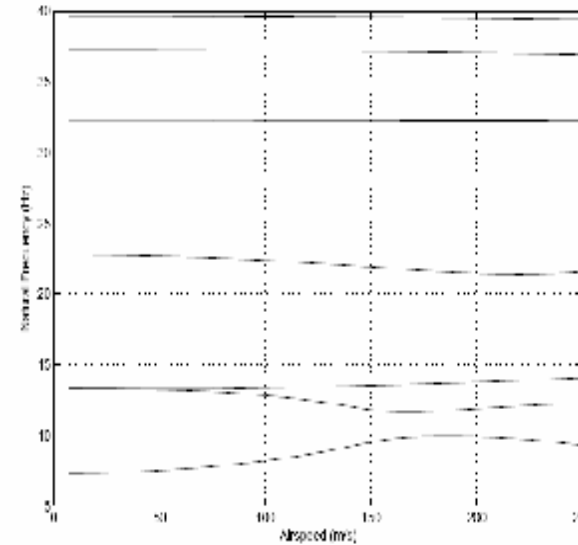
NC applied to full aircraft

- 9 structural modes
- 4 aerodynamic lag roots
- DOF-2-DOF cubic / freeplay non-linearity applied to control surface

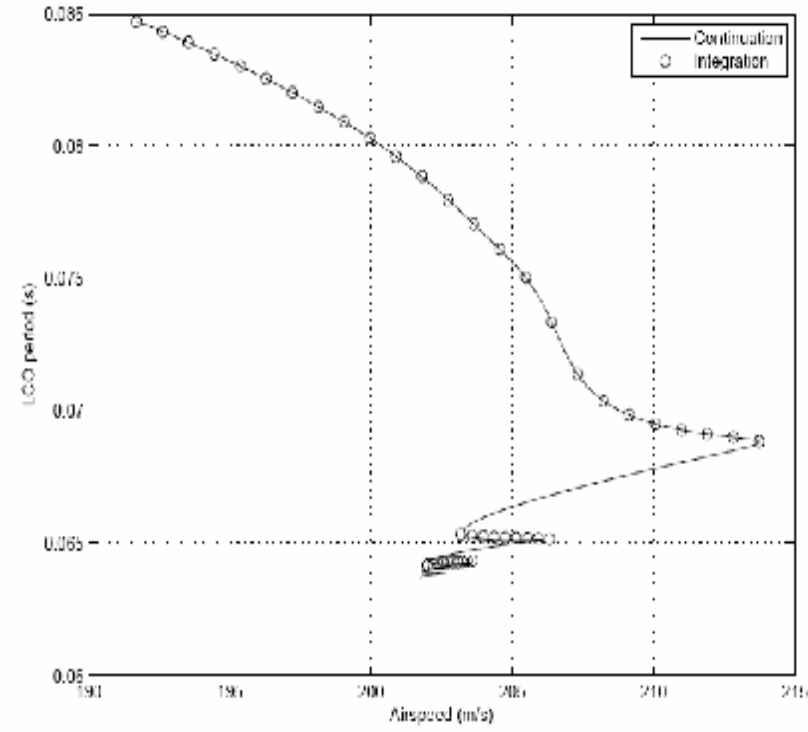
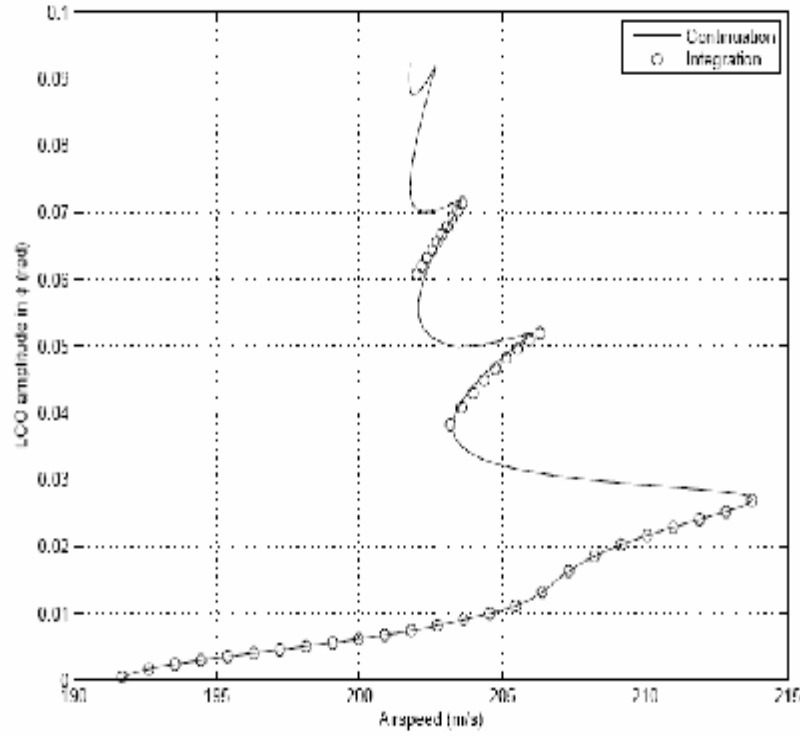


Frequency-damping plot

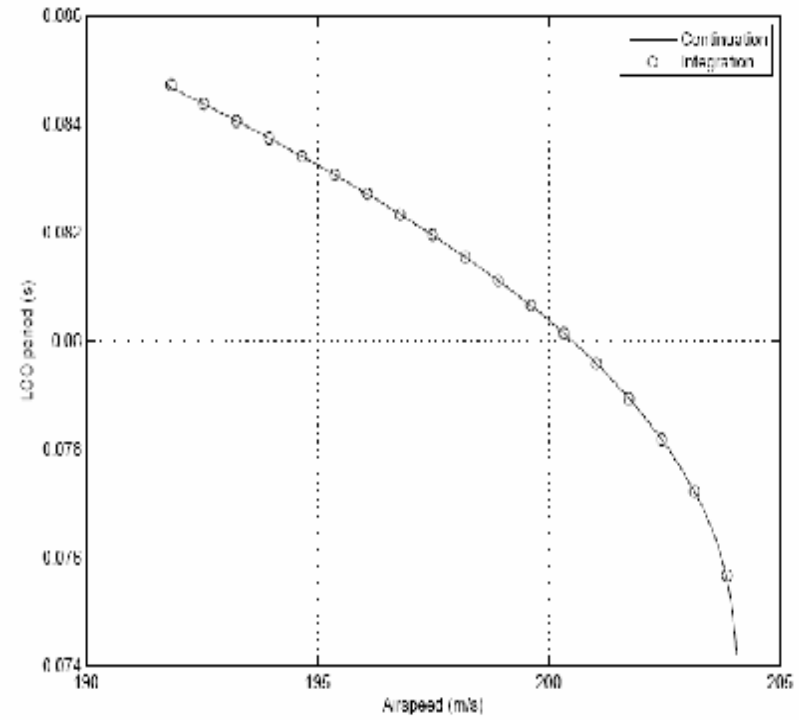
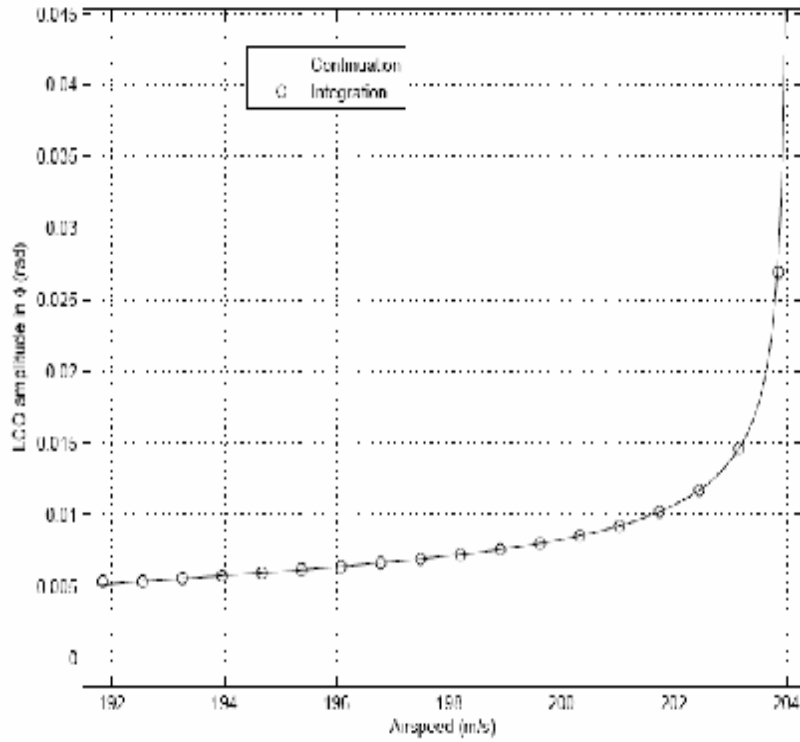
- M,C,K, AIC extracted from Nastran
- Roger approximation applied to transform AIC matrices to time domain



Cubic non-linearity



Freeplay non-linearity



Conclusions

- A number of different approaches have been described for modeling and prediction of linear and non-linear aeroelastic behaviour
- Prediction of non-linear aeroelastic phenomena presents a number of challenges for analysis, testing and FE/CFD modelling
- Further work involves the extension to larger order models and transonic aerodynamics